## Selection table for free oscillating systems (with unbalanced excitation)

|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | One mass system circular motion screen | One mass system linear motion screen | Two mass system with counterframe | One mass system linear motion screen hanging |
|  | $\begin{gathered} \text { AB } \\ \text { Page } \end{gathered}$ $2.11$ | Oscillating Mounting - universal mounting. <br> High vibration isolation and low residual force transmission. <br> Natural frequencies approx. $2-3 \mathrm{~Hz}$. <br> 9 sizes from 50 N to $20^{\prime} 000 \mathrm{~N}$ per AB . |  |  |  |
|  | AB-HD Page 2.12 | Oscillating Mounting for impact loading and high production peaks. (Heavy Duty) <br> Natural frequencies approx. $2.5-3.5 \mathrm{~Hz}$. 6 sizes from 500 N to $14^{\prime} 000 \mathrm{~N}$ per AB-HD. |  |  |  |
|  | AB-D Page 2.13 |  | Oscillating Mounting in compact design. Optimal in two mass systems as counterframe mounting. <br> Natural frequencies approx. $3-4.5 \mathrm{~Hz}$. 7 sizes from 500 N to $16^{\prime} 000 \mathrm{~N}$ per AB-D. |  |  |
|  | ABI <br> Page <br> 2.14 | Oscillating Mounting made from stainless steel for the food and pharmaceutical industry. <br> High vibration isolation and low residual force transmission. <br> Natural frequencies approx. $2-3 \mathrm{~Hz}$. <br> 6 sizes from 70 N to $6^{\prime} 800 \mathrm{~N}$ per ABI. |  |  |  |
|  | $\begin{gathered} \text { HS } \\ \text { Page } \\ 2.15 \end{gathered}$ |  |  |  | Oscillating Mounting for hanging systems. Natural frequencies approx. $3-4 \mathrm{~Hz}$. 5 sizes from 500 N to $14^{\prime} 000 \mathrm{~N}$ per HS . |

## Selection table for gyratory sifters



## ROSTA

## Technology

Design layout and evaluation

| Subject | Symbol | - Example |
| :---: | :---: | :---: |
| Mass of the empty channel and drive | $\mathrm{m}_{0}$ | 680 kg |
| Products on the channel |  | 200 kg |
| of which approx. 50\% coupling* |  | 100 kg |
| Total vibrating mass* | m | 780 kg |
| Mass distribution: feed end | \% feed end | 33\% |
|  | \%discharge end | 67\% |
| Acceleration due to gravity | g | $9.81 \mathrm{~m} / \mathrm{s}^{2}$ |
| Load per corner feed end | Ffeed end | 1263 N |
| Load per corner discharge end | $F$ discharge end | 2563 N |
| - Element choice in example |  | 6x AB 38 |
| Working torque of both drives | AM | 600 kgcm |
| Oscillating stroke empty channel | swo | 8.8 mm |
| Oscillating stroke in operation | sw | 7.7 mm |
| Motor revolutions | $\mathrm{n}_{\text {s }}$ | 960 rpm |
| Centrifugal force of both drives | Fz | $30^{\prime} 319 \mathrm{~N}$ |
| Oscillating machine factor | K | 4.0 |
| Machine acceleration | $a=K \cdot g$ | 4.0 g |
| - Natural frequency suspensions | fe | 2.7 Hz |
| Degree of isolation | W | 97\% |



## Calculation formulas

## Loading per corner

$$
F_{\text {feed-end }}=\frac{\mathrm{m} \cdot \mathrm{~g} \cdot \% \text { feed-end }}{2 \cdot 100} \quad \mathrm{~F}_{\text {discharge-end }}=\frac{\mathrm{m} \cdot \mathrm{~g} \cdot \% \text { discharge-end }}{2 \cdot 100}
$$

## Oscillating stroke (Amplitude peak to peak)

$$
s W_{0}=\frac{A M}{m_{0}} \cdot 10 \quad s W=\frac{A M}{m} \cdot 10
$$

## Centrifugal force

$$
F_{z}=\frac{\left(\frac{2 \pi}{60} \cdot n_{s}\right)^{2} \cdot A M \cdot 10}{2 \cdot 1000}=\frac{n_{s}^{2} \cdot A M}{18^{\prime} 240}
$$

## Oscillating machine factor

$K=\frac{\left(\frac{2 \pi}{60} \cdot n_{s}\right)^{2} \cdot s w}{2 \cdot g \cdot 1000}=\frac{n_{s}^{2} \cdot s w}{1^{\prime} 789^{\prime} 000}$


* The following has to be observed for the determination of the coupling effect and material flow:
- High coupling or sticking of humid bulk material
- Channel running full
- Fully stacked screen deck with humid material
- Weight distribution with and without conveyed material
- Centrifugal force does not run through the center of gravity (channel full or empty)
- Sudden impact loading occurs
- Subsequent additions to the screen structure (e.g. additional screening deck)



## Technology

## Determination of the average material conveying speed vm



## Main influencing factors:

- Conveying ability of the material
- Height of the bulk goods
- Screen box inclination
- Position of unbalanced motors
- Position of the center of gravity

The material speed on circular motion screens does vary, due to differing screen-box inclination angles.

## - Example:

The horizontal line out of the intercept point of stroke ( 7.7 mm ) and motor revolutions (960 rpm) is indicating an average theoretical speed of $12.3 \mathrm{~m} / \mathrm{min}$ or $20.5 \mathrm{~cm} / \mathrm{sec}$.

## Resonance amplification and continuous running

At the screen start-up and run-out the suspension elements are passing through the resonance frequency. By the resulting amplitude superelevation the four rubber suspensions in the $A B$ mountings do generate a high level of damping which is absorbing the remaining energy after only a few strokes. The screen box stops its motion within seconds.

Laboratory measurements of a typical development of the residual forces on a ROSTA screen suspension:


## Alignment of the elements

If the suspensions for linear motion screens are arranged as shown on page 2.7, a harmonic, noiseless oscillation of the screen will result. The rocker arm fixed to the screen carries out the greater part of the oscillations. The rocker arm fixed to the substructure remains virtually stationary and ensures a low natural frequency, and thereby also a good vibration isolation. The mounting axis has to be arranged to be at right angles $\left(90^{\circ}\right)$ to the conveying axis, with maximum tolerance of $\pm 1^{\circ}$.





## Deflection curves and cold flow behaviours

Diagrams showing the vertical deflection $\mathbf{s}$ (in mm ) by compression or tensile load G (in kN). The shown values comprehend the initial cold flow settling after one day of operation. The final element deflection after the full cold flow compensation (after approx. 1 year) is usually factor x 1,09 higher (depending on specific application, climate etc.).

## Final element deflection

$=\mathbf{s} \times 1,09$

The deflection values are based on our catalogue specifications and should be understood as approximate values. Please consult also our tolerance specifications in chapter "Technology" in the general catalogue.

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## Oscillating Mountings

## Type HS



| Art. No. | Type | Load capacity Gmin. - Gmax. <br> [ N ] |  | $\begin{aligned} & \mathrm{A}^{*} \\ & \text { max. } \\ & \text { load } \end{aligned}$ |  | $B^{*}$ <br> max. load | C | D | E | F | H | K | L | M | N | Weight [kg] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07311001 | HS 27 | $500-1 ' 250$ | 164 | 202 | 84 | 68 | 70 | 11 | 80 | 105 | 4.5 | 17 | 60 | 80 | 35 | 1.6 |
| 07311002 | HS 38 | 1'200-2'500 | 223 | 275 | 114 | 92 | 95 | 13 | 100 | 125 | 6 | 21 | 80 | 104 | 40 | 4.9 |
| 07311003 | HS 45 | 2'000 - 4'200 | 265 | 325 | 138 | 113 | 110 | $13 \times 20$ | 115 | 145 | 8 | 28 | 100 | 132 | 65 | 11.3 |
| 07311004 | HS 50 | 3'500 - 8'400 | 288 | 357 | 148 | 118 | 120 | $17 \times 27$ | 130 | 170 | 12 | 40 | 120 | 165 | 60 | 20.2 |
| 07311005 | HS 50-2 | 6'000-14'000 | 288 | 357 | 148 | 118 | 120 | $17 \times 27$ | 130 | 170 | 12 | 45 | 200 | 250 | 70 | 34.0 |



## c <br> for HS 50 according 2006/42/EG (hanging load bearing capacities)

The HS Mountings shall be fastened with the foreseen amount of screws (existing fixation holes or slots) of quality 8.8 with consideration of the prescribed fastening torque.

These types can be combined with one another (identical heights and operation behaviour)

* tensile load Gmax. and final cold flow compensation (after approx. 1 year).
** separate assembly instructions are available, please ask for details.

