

# Selection table for guided systems (crank driven)

				
<b>One mass shaker</b> "brute-force" system	<b>One mass shaker</b> "natural frequency" system	<b>Two mass shaker</b> "fast-runner" system with reaction force-compensation		
<b>Single Rocker</b> with adjustable length. Models with right-hand and left-hand threads. 7 sizes up to 5'000 N per rocker suspension.			<b>AU</b> Page 2.25	
<b>Single Rocker</b> with decided center distance. 6 sizes up to 2'500 N for flange fixation. 6 sizes up to 2'500 N for central fixation.			<b>AS-P</b> <b>AS-C</b> Page 2.26	
		<b>Double Rocker</b> with decided center distance. 5 sizes up to 2'500 N for flange fixation. 4 sizes up to 1'600 N for central fixation.	<b>AD-P</b> <b>AD-C</b> Page 2.27	
<b>Single Rocker</b> with adjustable length. Models with right-hand and left-hand threads. 7 sizes up to 5'000 N per rocker suspension.			<b>AR</b> Page 2.28	
<b>Drive Head</b> for crank drive transmission in shaker conveyors. Models with right-hand and left-hand threads. 9 sizes up to 27'000 N per drive head.			<b>ST</b> Page 2.29	
	<b>Spring Accumulator</b> with high dynamic spring value for feeder systems running close to resonance frequency. A spring accumulator consists of 2 DO-A elements. 5 sizes up to dynamic spring value of 320 N/mm.		<b>DO-A</b> Page 2.30	

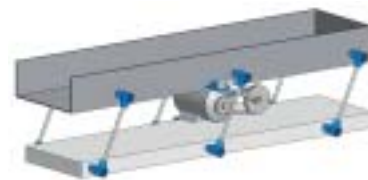
Notes regarding some special shaker systems:

- For free oscillating systems on pages 2.16–2.19
- For guided systems on pages 2.31 – 2.33
- For gyratory sifters on page 2.34



# Technology

## 1. One mass systems without spring accumulators: Calculation



### Calculation formulas

#### Oscillating machine factor

$$K = \frac{\left(\frac{2\pi}{60} \cdot n_s\right)^2 \cdot R}{g \cdot 1000} = \frac{n_s^2 \cdot R}{894'500}$$

#### Total spring value (machine)

$$c_t = m \cdot \left(\frac{2\pi}{60} \cdot n_s\right)^2 \cdot 0.001$$

#### Quantity of rockers

$$z = \text{round up} \left( \frac{L}{L_{\max}} + 1 \right) \cdot 2$$

#### Load per rocker

$$G = \frac{m \cdot g}{z}$$

#### Acceleration force (ST selection)

$$F = m \cdot R \cdot \left(\frac{2\pi}{60} \cdot n_s\right)^2 \cdot 0.001 = c_t \cdot R$$

#### Drive capacity approx.

$$P = \frac{F \cdot R \cdot n_s}{9550 \cdot 1000 \cdot \sqrt{2}}$$

#### Dynamic spring value per rocker

$$c_d = \frac{M_{d_d} \cdot 360 \cdot 1000}{A^2 \cdot \pi}$$

#### Resonant ability factor

$$i = \frac{z \cdot c_d}{c_t}$$

	Subject	Symbol	Example
Length, weight	Trough length	L	2.5 m
	Weight empty trough	m <sub>0</sub>	200 kg
	Weight of feeding material		50 kg
	Material coupling factor 50% *	m <sub>m</sub>	25 kg
	Weight of oscillating mass *	m = m <sub>0</sub> + m <sub>m</sub>	225 kg
Drive parameter	Eccentric radius	R	12 mm
	Stroke	sw = 2 · R	24 mm
	Rpm on trough	n <sub>s</sub>	340 min <sup>-1</sup>
	Gravity acceleration	g	9.81 m/s <sup>2</sup>
	Oscillating machine factor	K	1.6
	Acceleration	a = K · g	1.6 g
	Total spring value of system	c <sub>t</sub>	285 N/mm
Rocker arms	Distance between rockers max.	L <sub>max</sub>	1.5 m
	Quantity of rockers	z	6
	Load per rocker	G	368 N
	<b>Selection osc. elements (e. g.)</b>		<b>12x AU 27</b>
	<b>Selection ROSTA-elements: AU, AR, AS-P, AS-C</b>		
Center distance of elements	A	200 mm	
Drive	Acceleration force	F	3423 N
	<b>Selection drive head</b>		<b>1x ST 45</b>
Drive capacity approx.	P	1.0 kW	
Spring value	Dynamic torque	M <sub>d_d</sub>	2.6 Nm/°
	Dynamic spring value per rocker	c <sub>d</sub>	7.4 N/mm
	Dynamic spring value of all rockers	z · c <sub>d</sub>	44.7 N/mm
	Resonant ability factor	i	0.16

\* the following factors have to be considered by the definition of the material coupling:

- high coupling factor or sticking of wet and humid material
- possible stemming of the trough

## 2. One mass system with spring accumulators: Calculation

Calculation analog chapter 1 with following additions:



#### Resonant ability factor with accumulators

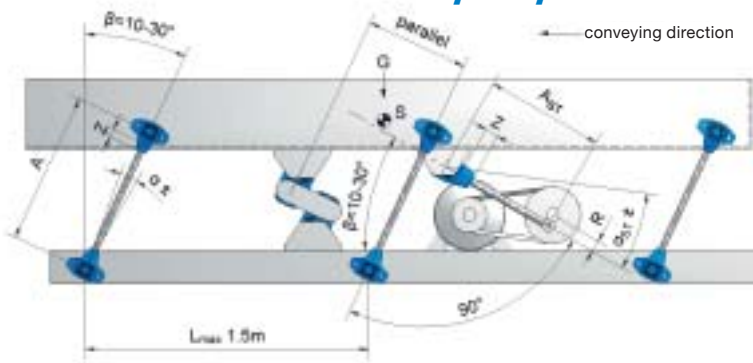
$$i_s = \frac{z \cdot c_d + z_s \cdot c_s}{c_t}$$

By a resonant ability factor  $i_s \geq 0.8$  the system is usually titled "natural frequency shaker".

Spring accumulators	Quantity	z <sub>s</sub>	2
	Dyn. spring value per item	c <sub>s</sub>	100 N/mm
	Dyn. spring value of all items	z <sub>s</sub> · c <sub>s</sub>	200 N/mm
	Resonant ability factor	i <sub>s</sub>	0.86
	<b>Selection of accumulators</b>		<b>2x cons. of 2x DO-A 45 x 80</b>

# Technology

## 3. One mass shaker conveyor systems: Installation instructions



### Distance between rockers $L_{max}$ :

- Usually, the distance between the rocker arms on the trough along-side is up to 1.5 meters, depending on the stiffness of the trough.
- By trough widths >1.5 m we do recommend to provide the trough bottom side with a third, central row of rocker arms for stability reasons.

### Mounting position drive head ST:

For one mass shaker systems it is recommendable to position the drive head slightly ahead of the center of gravity of the trough, towards the discharge end.

### Rocker mounting angle $\beta$ :

According to the relevant processing function of the shaker conveyor, the rocker arms are positioned at mounting angles between  $10^\circ$  to  $30^\circ$  in relation to the perpendicular line. (The ideal combination of fast conveying speed with high material throw is given by a rocker inclination angle of  $30^\circ$ .) The power input position of the drive-rod from the eccentric drive should stay at right angles to the rocker arms, this orthogonal positioning offers a harmonic course of the drive system.

### Angle of oscillation $\alpha$ :

The machine parameters, angle of oscillation and revolutions should be determined in the admissible area of operations (see chapter 5).

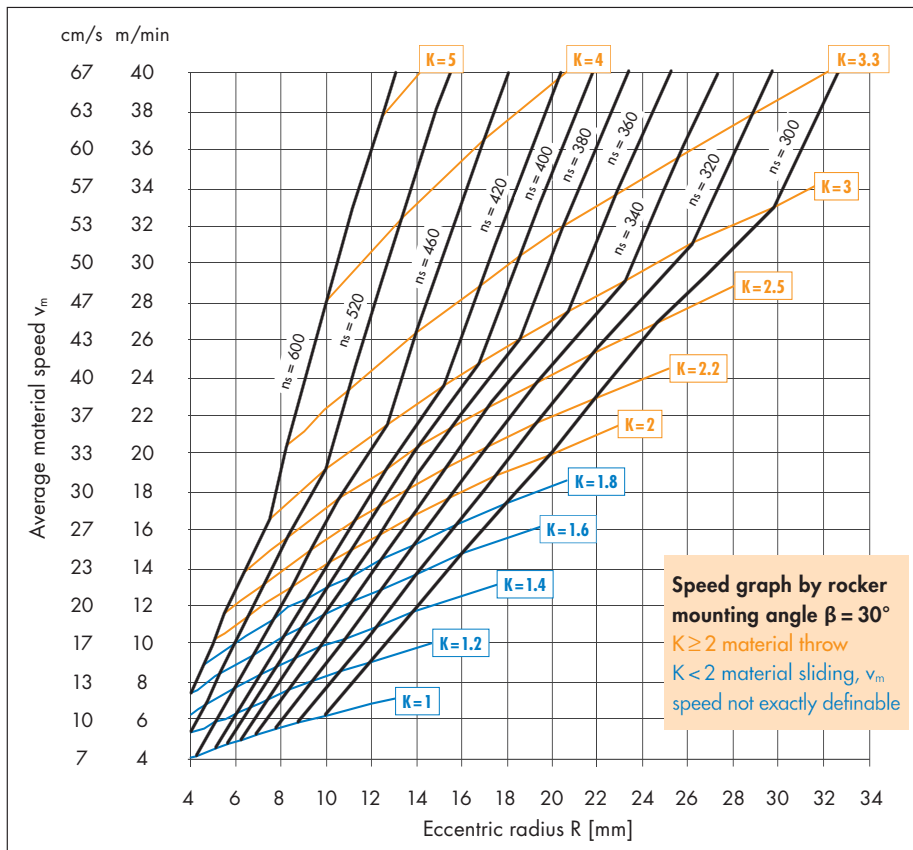
### Screw quality:

The screw quality should be grade 8.8 secured by the required tightening moment.

### Depth of thread engagement Z:

The depth of engagement should be at least 1.5 x the thread nominal width.

## 4. Average material speed on shakers $v_m$



### Main influence factors

- layer height of material
- property trough bottom (slip-resistance)
- mounting angle  $\beta$  of the rockers
- feeding capability of the material depending on size, form and humidity of the grains, e.g. very dry and fine grained material is submitted to slippage factors up to 30%.

### Example: One mass system with eccentric drive

Out of the intersection point  $R = 12 \text{ mm}$  and the revolutions  $n_s = 340 \text{ min}^{-1}$  is resulting a theoretical material speed of  $v_m = 12 \text{ m/min}$  or  $20 \text{ cm/sec}$ .

By acceleration factors  $K > 2$  and rocker mounting angles of  $\beta = 30^\circ$  (to the perpendicular line) the vertical acceleration is getting bigger than  $1g$ , therefore the material starts lifting from the trough bottom = material throw.

# Technology

## 5. Maximum rocker load $G$ , revolutions $n_s$ , and angle of oscillation $\alpha$

Size (e.g. AU 15)	max. load capacity per rocker [N]				max. revolutions $n_s$ [min <sup>-1</sup> ]*	
	K < 2	K = 2	K = 3	K = 4	$\alpha \pm 5^\circ$	$\alpha \pm 6^\circ$
15	100	75	60	50	640	480
18	200	150	120	100	600	450
27	400	300	240	200	560	420
38	800	600	500	400	530	390
45	1'600	1'200	1'000	800	500	360
50	2'500	1'800	1'500	1'200	470	340
60	5'000	3'600	3'000	2'400	440	320

The angle of oscillation  $\alpha$  of each oscillating component (rockers accumulators and drive head) has to be settled within the permissible range ( $n_s$  and  $\alpha$ ).

### Calculation oscillation angle for rockers

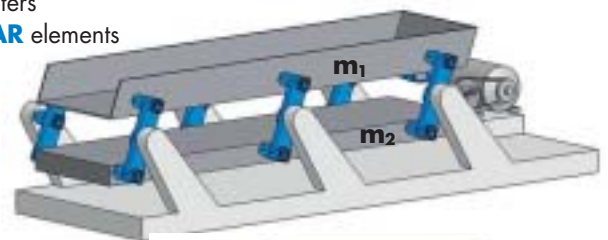
Eccentric radius R [mm]  
Center distance A [mm]      $\alpha = \arctan\left(\frac{R}{A}\right)$   
Oscillation angle  $\alpha \pm [^\circ]$

Please contact ROSTA for the permissible load indications by higher accelerations and for rocker elements offering higher load capacities. Usually are the revolutions  $n_s$  between 300 to 600 min<sup>-1</sup> and the oscillation angles max.  $\pm 6^\circ$ .

\* basics: "permissible frequencies" in the Technology part of the ROSTA catalogue.

## 6. Two mass shaker systems with direct reaction force-compensation

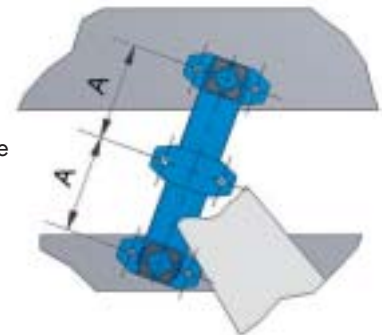
- Maximum acceleration forces of approx. 5 g, shaker lengths up to 20 meters
- Equipped with ROSTA double rockers **AD-P**, **AD-C** and/or made out of **AR** elements
- Ideal compensation when  $m_1 = m_2$
- Element selection analogue chapter 1, but with load of the two masses:  
Actuated mass (+ material coupling of feeding mass)  $m_1$  [kg]  
Driven mass (+ material coupling of feeding mass)  $m_2$  [kg]  
Total oscillating mass  $m = m_1 + m_2$  [kg]



Dynamic spring value  $c_d$  per double rocker

$$c_d = \frac{3 \cdot M_{d1} \cdot 360 \cdot 1000}{2 \cdot A^2 \cdot \pi} \text{ [N/mm]}$$

- Calculation of  $c_d$  and F based on the total mass ( $m_1$  and  $m_2$ )
- Power input from eccentric drive with **ST arbitrary** on  $m_1$  or  $m_2$  at **any point** alongside  $m_1$  or  $m_2$
- On demand, special double rocker arms with varying center distances A are available as "customized rockers"



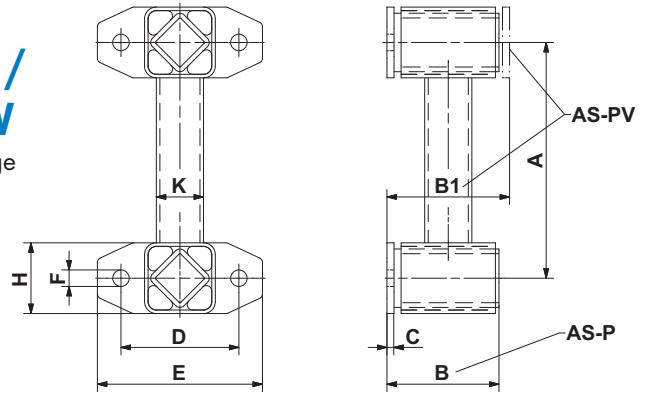
### The 9 installation steps for a two mass system with double rocker arms:

1. All fixation holes for the rockers in trough, counter-mass and machine frame have to be drilled very accurately previous the final machine assembling.
2. Installation of the middle elements of the rocker arms on the central machine frame, all inclination angles duly adjusted (e.g. 30°), tightening of the screws with required fastening torque.
3. Lifting of the counter-mass with accurate horizontal alignment until the bores in the counter-mass frame stay congruent with the bore holes of the lower element. Jamming of the counter-mass with e.g. wooden chocks.
4. Tightening of the fixation screws on counter-mass with required fastening torque.
5. Inserting of the feeding trough into machine frame structure. Accurate horizontal alignment until the bores in the trough stay congruent with the bore holes of the upper element. Jamming of the trough with e.g. wooden chocks.
6. Tightening of the fixation screws on trough with required fastening torque.
7. Installation of the driving rod with drive head ST in "neutral" position i.e. eccentric drive should stay in between the two stroke ends. Length adjustment of the driving rod and tightening of the counter-nuts.
8. Removal of the jamming chocks under counter-mass and trough.
9. Test start of the shaker conveyor.



## Single Rockers

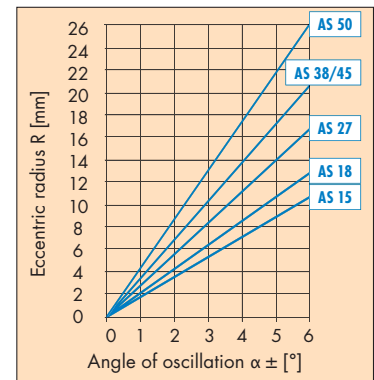
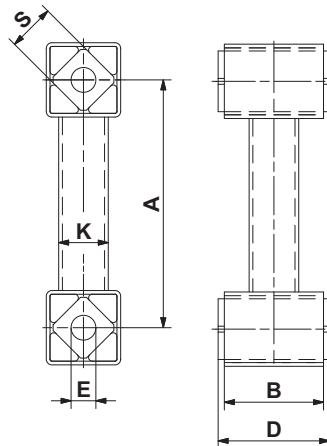
**AS-P / AS-PV**  
for flange fixation



Type AS-PV with inverted flange

Art. No.	Type	G [N] K<2	cd [N/mm]									Weight [kg]	Material structure
				A	B	B1	C	D	E	øF	H		
07 081 001	AS-P 15	100	5	100	50	-	4	50	70	7	25	18	Steel welded constructions, ROSTA blue painted
07 091 001	AS-PV 15				-	56							
07 081 002	AS-P 18	200	11	120	62	-	5	60	85	9.5	35	24	
07 091 002	AS-PV 18				-	68							
07 081 003	AS-P 27	400	12	160	73	-	5	80	110	11.5	45	34	
07 091 003	AS-PV 27				-	80							
07 081 004	AS-P 38	800	19	200	95	-	6	100	140	14	60	40	
07 091 004	AS-PV 38				-	104							
07 081 005	AS-P 45	1'600	33	200	120	-	8	130	180	18	70	45	
07 091 005	AS-PV 45				-	132							
07 081 006	AS-P 50	2'500	37	250	145	-	10	140	190	18	80	60	
07 091 006	AS-PV 50				-	160							

**AS-C**  
for frictional  
center connection



Art. No.	Type	G [N] K<2	cd [N/mm]							Weight [kg]	Material structure	
				A	B	D <sub>-0.3</sub>	øE	øK	□S		Inner square	Housing
07 071 001	AS-C 15	100	5	100	40	45	10 <sup>+0.4</sup> <sub>+0.2</sub>	18	15	0.4	Light metal profile	Steel welded construction, ROSTA blue painted
07 071 002	AS-C 18	200	11	120	50	55	13 <sup>0</sup> <sub>-0.2</sub>	24	18	0.6		
07 071 003	AS-C 27	400	12	160	60	65	16 <sup>+0.5</sup> <sub>+0.3</sub>	34	27	1.3		
07 071 004	AS-C 38	800	19	200	80	90	20 <sup>+0.5</sup> <sub>+0.2</sub>	40	38	2.6		
07 071 005	AS-C 45	1'600	33	200	100	110	24 <sup>+0.5</sup> <sub>+0.2</sub>	45	45	3.9		
07 071 006	AS-C 50	2'500	37	250	120	130	30 <sup>+0.5</sup> <sub>+0.2</sub>	60	50	6.1		

G = max. load in N per rocker, by higher K consult chapter 5 on page 2.24.  
cd = dynamic spring value by oscillation angles  $\alpha \pm 5^\circ$  in speed range of  $n_s = 300-600 \text{ min}^{-1}$

Further basic information and calculations on pages 2.22-2.24.